



## Impact of stem-broach sizing on the cement mantle of Lubinus SP II stems. A CT scan analysis

Thierry SCHEERLINCK, Johan DE MEY, Rudi DEKLERCK

*From the VUB University Hospital, UZ Brussel, Belgium*

Lubinus SP II stems are cemented either line-to-line with the largest broach or one-size undersized. The purpose of this study was to compare both implantation techniques. We used 18 polymeric stem replicas cemented line-to-line and undersized in paired cadaveric femora and analyzed them with CT scan images. Cementing Lubinus stems line-to-line resulted in higher medullary canal-filling indices ( $28.26 \pm 4.10\%$ ), thinner cement mantles ( $3.29 \pm 0.40$  mm), more cement defects ( $5.12 \pm 1.69\%$ ) and more areas of thin cement ( $23.81 \pm 7.13\%$ ) than undersizing (respectively :  $23.61 \pm 4.24\%$ ,  $3.62 \pm 0.43$  mm,  $1.48 \pm 2.04\%$ ,  $15.11 \pm 5.93\%$ ). In both settings, over 80% of areas of thin or deficient cement were supported by cortex. Using a line-to-line technique, adequate stem alignment was achieved without distal centralizer. Undersizing the stem and using a distal centralizer reduced the incidence of distal cement defects by a factor 10. While stems cemented line-to-line might have mechanical advantages, undersizing and using distal centralizers reduced potential pathways for debris migration to the bone-cement interface.

**Keywords :** hip arthroplasty ; femoral stem ; cement mantle ; Lubinus SP2 ; computed tomography ; cementing technique.

### INTRODUCTION

The cement mantle surrounding femoral hip implants acts as a mechanical interface between stem and bone (2,14) and limits the possibilities of debris migration to the femoral canal (1,8). As such,

a uniform and substantial cement mantle without defects, that is well anchored into cancellous bone and well supported by cortical bone, should be adequate. In order to avoid areas of thin or deficient cement, some manufacturers have developed implants which try to match the inner proximal femoral anatomy (3,17). The Lubinus SP II stem (Status Physiologus, Waldemar Link GmbH, Hamburg, Germany) is one of these “anatomic” cemented stems. It is asymmetric, and has a left and a right version with a characteristic S-shaped curvature in the lateral view, a large collar and a femoral neck with  $19^\circ$  of anteversion (fig 1). It is made of

---

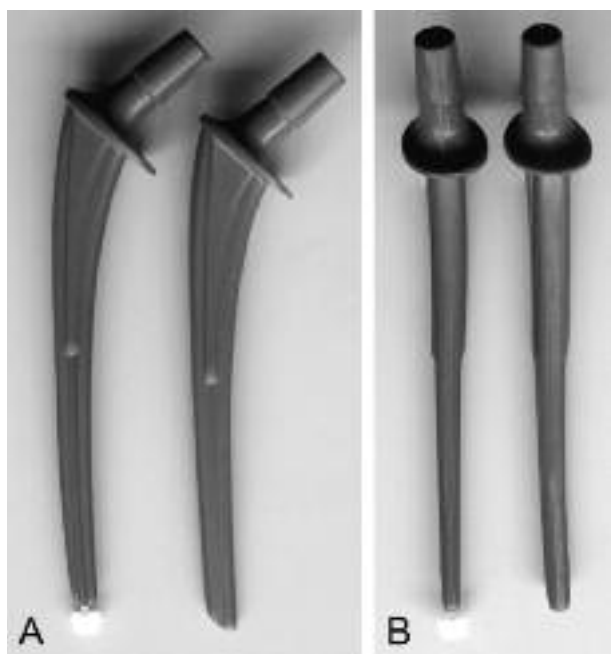
■ Thierry Scheerlinck, MD, PhD, Senior Staff Surgeon.  
*Department of Orthopaedic Surgery, Universitair Ziekenhuis Brussel, Belgium.*

■ Johan de Mey, MD, PhD, Professor of Radiology.  
*Department of Radiology, Universitair Ziekenhuis Brussel, Belgium.*

■ Rudi Deklerck, Eng, PhD, Postdoc Researcher.  
*Department of Electronics and Informatics (ETRO), Research Group IRIS, Vrije Universiteit Brussel (VUB), Interdisciplinair Instituut voor BreedBandTechnologie (IBBT), Belgium.*

Correspondence : Thierry Scheerlinck, Department of Orthopaedic Surgery and Traumatology, Universitair Ziekenhuis Brussel, Laarbeeklaan 101, 1090 Brussels, Belgium. E-mail : [Thierry.Scheerlinck@uzbrussel.be](mailto:Thierry.Scheerlinck@uzbrussel.be)

© 2009, Acta Orthopædica Belgica.



**Fig. 1.** — Anteroposterior (A) and lateral (B) view of polymeric replicas of the Lubinus SP II stem. The undersized stem was instrumented with a distal centralizer (left); the line-to-line stem was implanted without distal centralizer (right).

cobalt-chrome with a satin to matte surface finish ( $R_a = 0.39$  to  $1.4 \mu\text{m}$ ) (4,5). The Lubinus stem is widely used throughout Europe (16). Overall, clinical and experimental results have been favourable (6,10,11,13,15,21).

To further “optimize” the cement mantle, manufacturers proposed to undersize (US) the stem compared to the broach. However, many implants that are cemented line-to-line (LL) with the largest broach have been very successful (9,17,20). The surgical technique of the Lubinus SP II stem allows both implantation philosophies. According to the manufacturer, both techniques are widely used, but it is unknown, which is superior and what the implications are for the stem-cement-bone composite.

We used a validated CT scan based measurement tool (18) to analyze the effect of the line-to-line and undersized implantation of an “anatomic” Lubinus SP II stem on the cement mantle quality. We compared both implantation techniques, focusing on

mechanically and/or biologically relevant parameters. When differences were found, their potential implications were evaluated.

## MATERIALS AND METHODS

### Stem implantation technique

Eighteen polymeric replicas of the Lubinus SP II stem (fig 1), provided by the manufacturer, were implanted in nine pairs of embalmed cadaver femora. An experienced hip surgeon (T.S.) and an experienced theatre nurse (C.V.P.) performed all implantations with original instruments, according to the recommended surgical technique and simulating a realistic intra-operative setting. Radiographic templating was performed on anteroposterior and lateral views and nine pairs of femora suitable for a stem size 2 or 3 were selected. The femoral neck was cut according to templating. Flexible reamers were used to open the medullary canal until cortical contact was achieved. Subsequently, broaches of increasing size were used to prepare the femoral canal according to templating and until the largest possible broach was inserted. Both femora from the same donor were reamed and broached to the same size and a calcar planer was used in all cases. Four pairs of small femora were reamed to 12 mm and broached with a size 2 broach. Five pairs of larger femora were reamed to 14 mm and broached with a size 3 broach. At one side, we implanted a stem replica with the same size as the broach (line-to-line technique). At the other side, a one-size undersized replica was used. Undersized replicas were instrumented with an in-stem distal centralizer (PMMA Invis™ distal post centralizer, Smith & Nephew, Memphis, Tennessee, USA) of 10 mm for stems size 1 and of 11 mm for stems size 2. Sides were allocated randomly.

We applied a third generation cementing technique including the use of a distal cement plug and cleansing of the femoral canal with 2 l of water at  $37^\circ\text{C}$  with a pressure lavage system (Stryker, Mahwah, New Jersey, USA). Eighty gram of polymethylmethacrylate cement (Palamed, Biomet, Warsaw, Indiana, USA) was vacuum mixed (30 s, 0.1 bar) at  $18^\circ\text{C}$  with a mixing/pressurizing system (Optivac, ScandiMed, Biomet, Warsaw, Indiana, USA) and injected into the femoral canal, 3 minutes after starting the mixing. Cement was pressurized with a proximal seal during 1 minute. At 4 minutes, the stem replica was inserted manually until the collar contacted the calcar cut. Pressure was maintained during stem insertion and until complete setting of the cement.

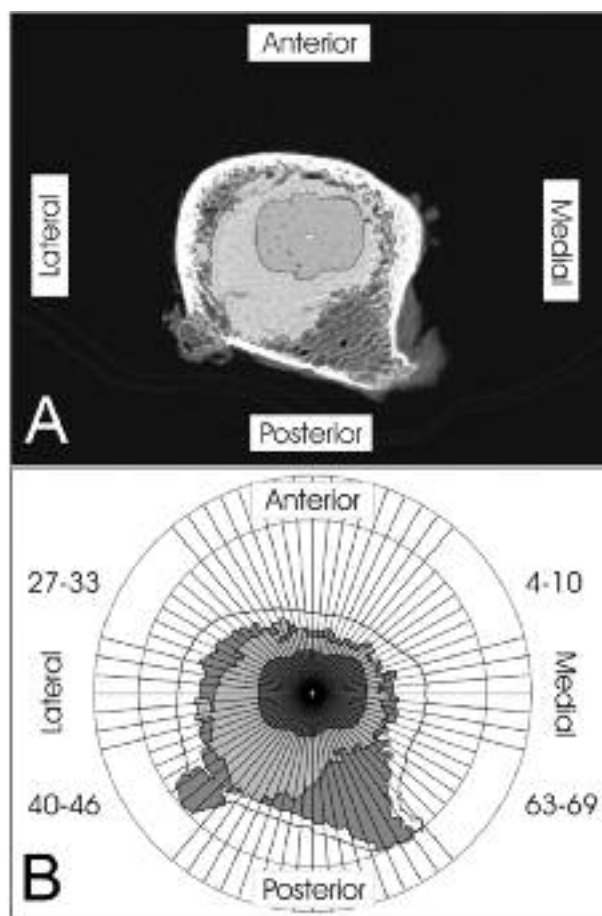
## Data analysis

All specimens were scanned with a Somatom Sensation 16 CT scanner (Siemens AG, Erlangen, Germany) using the following settings : adjacent slices ; collimation :  $6 \times 0.75$  mm ; slice thickness : 1.0 mm ; reconstructed slice interval : 0.5 mm and reconstruction kernel : 80U very sharp. Specimens were positioned based on the CT laser beam and scanned along their longitudinal axis. In total 4978 images (LL : 2483, US : 2495) were reconstructed from the medial calcar cut to the distal stem tip.

Validated custom segmentation software (18) identified the contours of the cement mantle, the outer and the inner cortex, according to their gray values in the CT image. Differences in gray values between the polymeric stem replica and the cement could be distinguished visually but were too small for easy automated segmentation. For this, implants were CT scanned and segmented separately, and the contours were fitted to the stem in corresponding CT images of the specimens.

Based on their contours, the volumes of the four elements (cortical and cancellous bone, cement and prosthesis) were calculated by multiplying the cross-sectional area of an element by the slice interval and by integrating these volumes over consecutive CT images. The mean degree of centralization of two elements within one specimen was calculated by averaging the distances between their centroids over consecutive images. The “canal-filling index” of an element was defined as : (volume of an element) / (volume of medullary canal)  $\times 100$ . Global stem alignment with respect to the medullary canal was evaluated by calculating the angle between the line of best fit to the centroids of the medullary canal and the line of best fit to the centroids of the stem (19). Both lines were calculated in a region starting 1 cm above the stem tip and extending for 8 cm proximally. The varus-valgus tilt and anteroposterior tilt were defined as the angles between both lines, after projection onto the frontal and sagittal plane respectively.

The cancellous bone thickness was calculated in the CT scan plane, while the cement mantle thickness was calculated in 3D (18,19). For each CT image, the cement mantle thickness (including cement pressurized into cancellous bone) and the cancellous bone thickness were averaged in 72 segments of  $5^\circ$  around the prosthesis centroid. In total, both parameters were analyzed in 358,416 (LL : 178,776 ; US : 179,640) segments. Segments with a mean cement thickness  $< 1$  mm were defined as “cement mantle defects”, segments with a mean thickness  $< 2$  mm as “areas of thin cement”. Within each



**Fig. 2.** — Segmented CT scan image of a Lubinus SP II replica cemented in a donor femur (A). Reconstructed image based on the segmentation procedure (B). The image was divided in 72 segments of  $5^\circ$  around the prosthesis centroid. Segments 4 to 10, 27 to 33, 40 to 46 and 63 to 69 represent corner regions ; the remaining segments represent flat regions of the stem.

CT image, twenty-eight segments were considered as “corner” regions of the stem’s cross-section, the remaining forty-four segments were considered as “flat” regions (fig 2).

## Statistical methods

We compared results of stems cemented LL and US in paired femora with a two-tailed paired samples Student’s t-test. The effect size ( $d = \text{Mean}[\text{differences between pairs}] / \text{SD}[\text{differences between pairs}] \times \sqrt{2}$ ) was calculated for each parameter (23). In contradiction to “statistical significance”, the “effect size” is independent from sample size and reflects the magnitude of the difference

between the line-to-line and undersized technique. An effect size  $> 0.8$  can be considered as "large". Setting the significance criterion (p-value) to 0.05 and using nine pairs of femora, the power was 80% when the effect size of the paired t-test reached 1.5. However, when the effect size of the paired t-test decreased to 1.0, the power dropped to 43%. Frequencies were compared with a Chi<sup>2</sup>-test. Statistical analysis was conducted with Excel 2000 (Microsoft Inc., Redmond, USA) and SPSS 13.0 (SPSS Inc., Chicago, USA). P-values  $< 0.05$  were considered statistically significant.

## RESULTS

The average radius of undersized stems was  $0.55 \pm 0.11$  mm smaller ( $p < 0.001$ ) than that of line-to-line stems (sizes 1-2 :  $0.64 \pm 0.04$  mm [ $p < 0.001$ ]; sizes 2-3 :  $0.47 \pm 0.08$  mm [ $p < 0.001$ ]). Overall, the Lubinus SPII stem filled  $25.94 \pm 4.70\%$  of the medullary canal. The volume and medullary canal-filling index of stems implanted line-to-line were larger than those of undersized stems. The amount of cement was similar in both settings (table I).

Stem centralization within the cement mantle and the medullary canal was similar in both groups (table II). In the distal 1/3, undersized stems instrumented with a distal centralizer were better centred, than line-to-line stems without centralizer. Overall, stem alignment within the distal femoral canal did not differ significantly between groups (table II). The maximal global misalignment was  $3.68^\circ$ . Only

one stem was misaligned more than  $3^\circ$  and this was an undersized stem. In the frontal plane, half the stems were in neutral position ( $< 1^\circ$  of varus or valgus). The remaining 9 stems (LL : 5, US : 4) were in varus between  $1.13^\circ$  and  $2.57^\circ$ . In the sagittal plane, 11/18 stems were in neutral position ( $< 1^\circ$  of anterior or posterior tilt). The remaining 7 stems (LL : 2, US : 5) presented an anterior tilt between  $1.06^\circ$  and  $2.70^\circ$ . All maximal values were found in the undersized group.

Stems inserted line-to-line had a thinner cement mantle than undersized stems, but differences were small ( $0.33 \pm 0.21$  mm) and were not significant in the proximal 1/3 of the specimens (table III). In both settings, the mean cement thickness in the proximal 1/3 ( $4.08 \pm 0.61$  mm) was larger than in the middle ( $3.11 \pm 0.45$  mm ;  $p < 0.001$ ) and the distal 1/3 ( $3.15 \pm 0.42$  mm ;  $p < 0.001$ ). The average cement thickness below the medial femoral neck cut was  $3.78 \pm 0.78$  mm and was similar in both settings (table III). Cement defects and areas of thin cement were more numerous after line-to-line implantation than in the undersized group, especially in the distal 1/3 (table III). However, even in the line-to-line setting, the amount of cement defects was limited ( $5.12 \pm 1.69\%$ ). In both settings, areas of thin or deficient cement were more frequent at the corners of the stem (defects LL : 8.33%, US : 2.69% ; thin cement LL : 32.93%, US : 21.93%) than in the flat regions (defects LL

Table I. — Average volume and average medullary canal-filling index ([volume of an element] / [volume of medullary canal]  $\times 100$ ) after "line-to-line" and "undersized" stem cementation

	Line-to-Line Mean (SD)	Undersized Mean (SD)	Diff. between pairs (LL-US)		p-values	ES**
			Mean (SD)	95% CI		
Total volume (cm <sup>3</sup> )	112 (14.33)	113 (14.42)	-1.05 (2.58)	-3.03 / 0.94	0.259	0.57
Volume of cortical bone (cm <sup>3</sup> )	51.7 (11.92)	51.5 (11.58)	0.25 (3.51)	-2.46 / 2.95	0.839	0.10
Volume of medullary canal (cm <sup>3</sup> )	59.9 (8.11)	61.2 (11.08)	-1.29 (4.64)	-4.86 / 2.27	0.427	0.39
Volume of stem (cm <sup>3</sup> )	16.7 (1.13)	14.1 (1.31)	2.57 (0.31)	2.33 / 2.81	$< 0.001^*$	11.71
Volume of cement (cm <sup>3</sup> )	25.3 (4.05)	26.4 (4.30)	-1.13 (2.52)	-3.07 / 0.80	0.214	0.64
Volume of remaining cancellous bone (cm <sup>3</sup> )	17.9 (4.82)	20.6 (7.86)	-2.73 (3.92)	-5.75 / 0.28	0.070	0.99
Canal-filling index of the stem (%)	28.26 (4.10)	23.61 (4.24)	4.65 (1.59)	3.43 / 5.87	$< 0.001^*$	4.14
Canal-filling index of the cement (%)	42.24 (2.94)	43.55 (4.51)	-1.31 (3.91)	-4.32 / 1.69	0.343	0.47
Canal-filling index of the cancellous bone (%)	29.50 (5.15)	32.83 (8.01)	-3.34 (4.19)	-6.55 / -0.12	0.044*	1.13

\* Paired t-test :  $p < 0.05$  is statistically significant. \*\* ES : Effect size for a paired t-test.

Table II. — Stem centralization within the cement mantle and medullary canal and stem alignment in the medullary canal

	Line-to-Line Mean (SD)	Undersized Mean (SD)	Diff. between pairs (LL-US)		p-values	ES**
			Mean (SD)	95% CI		
Overall stem / cement centralization (mm)	1.36 (0.74)	1.37 (0.92)	0.00 (0.54)	-0.41 / 0.42	0.947	0.01
Stem-cement proximal 1/3 (mm)	1.79 (0.48)	1.91 (0.74)	-0.12 (0.82)	-0.75 / 0.51	0.678	0.20
Stem-cement middle 1/3 (mm)	1.02 (0.62)	1.28 (0.66)	-0.27 (0.95)	-1.00 / 0.47	0.428	0.39
Stem-cement distal 1/3 (mm)	1.56 (0.57)	1.16 (0.30)	0.40 (0.47)	0.03 / 0.76	0.035*	1.19
Overall stem / medullary canal centralization (mm)	2.53 (0.55)	2.60 (0.91)	-0.07 (0.93)	-0.79 / 0.65	0.823	0.11
Stem-medullary canal proximal 1/3 (mm)	4.86 (0.85)	5.05 (1.28)	-0.19 (1.11)	-1.04 / 0.66	0.619	0.24
Stem-medullary canal middle 1/3 (mm)	1.10 (0.30)	1.51 (0.80)	-0.41 (0.91)	-1.11 / 0.29	0.216	0.63
Stem- medullary canal distal 1/3 (mm)	1.62 (0.37)	1.23 (0.28)	0.38 (0.34)	0.12 / 0.64	0.009*	1.60
Global tilt of the stem in the medullary canal (°)	1.52 (0.87)	1.79 (0.98)	-0.27 (0.90)	-0.96 / 0.43	0.395	0.42
Stem alignment in frontal plane (°)	1.16 (0.75)	1.31 (0.90)	-0.15 (0.70)	-0.68 / 0.39	0.551	0.29
Stem alignment in sagittal plane (°)	0.82 (0.71)	1.07 (0.74)	-0.24 (1.26)	-1.21 / 0.72	0.579	0.27

\* Paired t-test :  $p < 0.05$  is statistically significant. \*\* ES : Effect size for a paired t-test.

Table III. — Mean cement mantle and cancellous bone thickness after “line-to-line” and “undersized” stem cementation in three areas along the stem. Cement mantle “defects” and “areas of thin” cement as a percentage of 5° segments around the prosthesis centroid

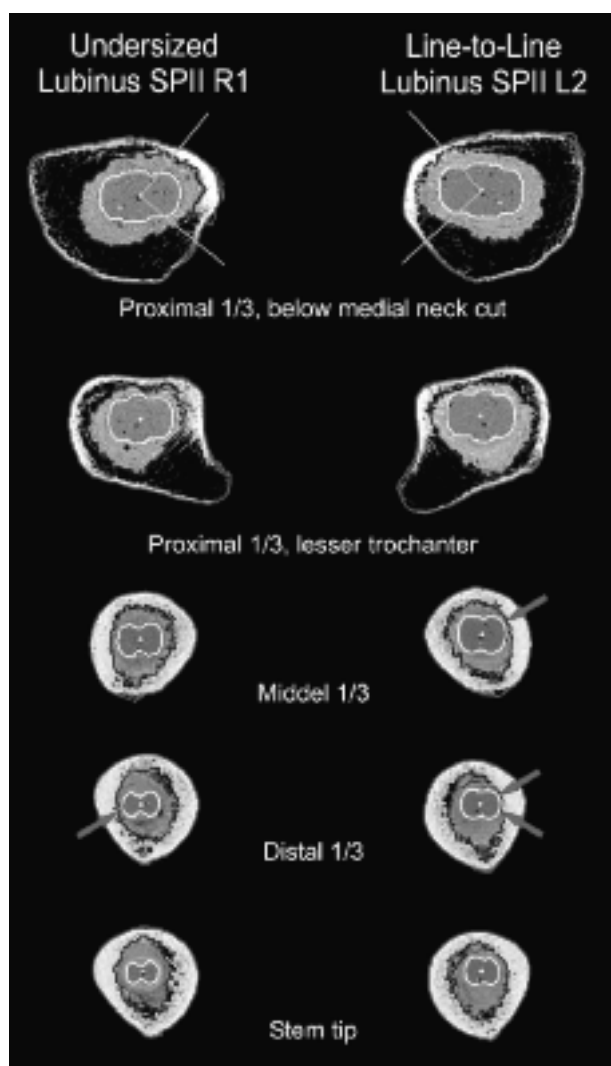
	Line-to-Line Mean (SD)	Undersized Mean (SD)	Diff. between pairs (LL-US)		p-values	ES**
			Mean (SD)	95% CI		
Overall cement mantle thickness (mm)	3.29 (0.40)	3.62 (0.43)	-0.33 (0.21)	-0.49 / -0.17	0.001*	2.26
Proximal 1/3 of stem (mm)	4.04 (0.69)	4.13 (0.54)	-0.09 (0.50)	-0.47 / 0.30	0.608	0.25
Middle 1/3 of stem (mm)	2.91 (0.32)	3.32 (0.48)	-0.41 (0.20)	-0.56 / -0.25	< 0.001*	2.89
Distal 1/3 of stem (mm)	2.89 (0.30)	3.41 (0.36)	-0.51 (0.13)	-0.61 / -0.41	< 0.001*	5.55
Cement thickness in calcar region (mm)	3.69 (1.07)	3.86 (0.89)	-0.17 (1.00)	-0.95 / 0.60	0.616	0.25
Overall prevalence of cement defects (< 1 mm) (%)	5.12 (1.69)	1.48 (2.04)	3.63 (2.34)	1.84 / 5.43	0.002*	2.20
Cement defects in proximal 1/3 (%)	2.16 (2.03)	1.19 (2.57)	0.97 (2.23)	-0.75 / 2.69	0.229	0.61
Cement defects in middle 1/3 (%)	4.54 (3.26)	2.45 (3.93)	2.09 (5.57)	-2.19 / 6.37	0.293	0.53
Cement defects in distal 1/3 (%)	8.80 (3.87)	0.83 (1.22)	7.97 (4.31)	4.66 / 11.29	0.001*	2.62
Overall prevalence of areas of thin cement (< 2 mm) (%)	23.81 (7.13)	15.11 (5.93)	8.70 (4.64)	5.13 / 12.27	< 0.001*	2.65
Thin cement in proximal 1/3 (%)	11.47 (7.50)	10.49 (8.07)	0.98 (6.06)	-3.66 / 5.62	0.640	0.23
Thin cement in middle 1/3 (%)	26.60 (11.07)	19.78 (7.79)	6.82 (10.71)	-1.41 / 15.05	0.092	0.90
Thin cement in distal 1/3 (%)	33.93 (6.78)	15.27 (8.54)	18.66 (7.32)	13.03 / 24.29	< 0.001*	3.60
Overall cancellous bone thickness (mm)	1.17 (0.33)	1.37 (0.57)	-0.20 (0.30)	-0.43 / 0.02	0.070	0.98
Proximal 1/3 of stem (mm)	2.91 (0.64)	3.39 (1.06)	-0.49 (0.55)	-0.91 / -0.06	0.030*	1.25
Middle 1/3 of stem (mm)	0.25 (0.20)	0.32 (0.31)	-0.07 (0.15)	-0.18 / 0.04	0.189	0.67
Distal 1/3 of stem (mm)	0.22 (0.23)	0.30 (0.34)	-0.07 (0.24)	-0.25 / 0.11	0.388	0.43
Cancellous bone thickness in calcar region (mm)	1.71 (1.39)	2.12 (1.23)	-0.41 (1.43)	-1.51 / 0.69	0.419	0.40
Cancellous bone thickness in areas of cement defects (mm)	0.47 (0.87)	1.59 (1.37)	-1.12 (1.27)	-2.09 / -0.14	0.029*	1.25
Cancellous bone thickness in areas of thin cement (mm)	0.46 (0.55)	1.00 (0.66)	-0.53 (0.46)	-0.89 / -0.18	0.009*	1.62

\* Paired t-test :  $p < 0.05$  is statistically significant. \*\* ES : Effect size for a paired t-test.

3.08%, US : 0.72% ; thin cement LL 18.01%, US 10.78%, Chi<sup>2</sup>-test :  $p$  all < 0.001).

Whatever implantation technique was used, cancellous bone between cortex and cement was found

almost exclusively in the proximal 1/3 of the specimens. Differences in cancellous bone thickness between line-to-line and undersized stems were small (< 0.5 mm) and were only significant in the



**Fig. 3.** — Segmented CT images of an undersized and a line-to-line Lubinus SP II replica implanted in both femora of the same donor. Proximally, below the medial femoral neck cut, large quantities of cement and cancellous bone were found in both cases. The stem implanted line-to-line presents more cement defects and areas of thin cement than the undersized stem (arrows). These areas were located mainly at the stem corners and were mostly supported by cortical bone. The tip of the undersized stem instrumented with a distal centralizer was better centred than the tip of the line-to-line stem implanted without centralizer.

proximal 1/3 (table III). The cancellous bone layer below the medial femoral neck cut was  $1.92 \pm 1.29$  mm thick and was independent from the implantation technique (table III). In areas of thin or deficient cement, line-to-line stems contained less

cancellous bone than undersized stems (table III). In both settings, over 80% of areas of thin or deficient cement were supported by cortex or  $< 1$  mm of cancellous bone.

## DISCUSSION

Currently, the Lubinus SP II stem is cemented either using an implant with similar dimensions as the largest possible broach (line-to-line technique) or using an undersized stem. Based on a validated CT scan evaluation technique (18), we compared morphometrical measurements of the stem-cement-bone composite resulting from both implantation philosophies (fig 3). Undersizing the stem and using a distal centralizer, produced a thicker cement mantle, less cement defects and less areas of thin cement compared to a stem cemented line-to-line without centralizer. As described previously (19,20), a third generation cementation technique can generate cement mantles over 3 mm thick, even after line-to-line implantation. Due to the small radial difference between stem sizes (0.55 mm) and to cement pressurization into cancellous bone, the impact of the surgical technique on the overall cement thickness was limited (0.33 mm). In the proximal 1/3 of the stem, where more cancellous bone was available, the cement mantle was thicker ( $> 4$  mm) and was independent from the implantation technique. However, more distally, cement pressurization was limited by cortical bone and differences were more marked.

The low canal-filling index of the Lubinus stem and the cement pressurization into retained cancellous bone can explain the low number of cement defects (5%) even after line-to-line implantation. In general, defects were associated with corner regions of the stem and were mostly supported by cortex. These regions corresponded to “point contacts” between stem and cortex in places where lack of cancellous bone limited cement interdigitation. Compared to a line-to-line implantation without distal centralizer, undersizing and using a distal centralizer, reduced the overall incidence of cement defects by at least a factor three but reduced the incidence of distal defects by a factor ten. That reduction might be important because cement

defects are potential pathways for particle migration and could be a source of distal osteolysis.

Stem alignment and stem centralization within the cement mantle and the femoral canal were similar in both groups. However, all “extreme” misalignments were found in the undersized group although these stems were better centred distally. This apparent contradiction resulted from the use of distal centralizers in the undersized group but not in the line-to-line group. They reduced the eccentricity of the small tip of undersized stems (canal-filling index < 25%), but could not always prevent global stem misalignment. Line-to-line stems without centralizer were guided by bony contacts in the proximal and middle third of the medullary canal. This provided an adequate alignment but could not prevent the eccentric location of the relative small stem tip (canal-filling index < 30%). As such a distal centralizer for the Lubinus SP II stem could be considered even in the line-to-line scenario.

In the region below the medial femoral neck cut and despite a tendency to varus stem positioning, the implant and the cortex were separated by 3.8 mm of cement and almost 2 mm of cancellous bone. This was independent from the implantation technique and was attributed to the straight proximal part of the medial border of the Lubinus stem. As the region below the medial femoral neck cut is subjected to high stresses, providing a thick cement layer in that region could be favourable (2,12,14). However, the presence of weak cancellous bone is detrimental (2,22). As such, it is advisable to curette superfluous cancellous bone, preserving a well-fixed layer of 2 or 3 mm for cement-bone interlock.

Although our CT scan based evaluation tool allows accurate *in vitro* measurements of the stem-cement-bone complex (18), it can be criticized. We assumed the left and right femur of a single donor to be “identical” and that is not always the case. However, in our study, the total volume, the amount of cortex and the volume of the medullary canal of paired specimens were all similar (table I). Moreover, we do not see an alternative way to compare two cementing techniques using human femora. Blood contamination and access impairment to the proximal femur caused by soft tissues, were not reproduced. This might result in a better cement

mantle than could be achieved in clinical practice. However, as the implantation circumstances were standardized, this does not impair the direct comparison of both surgical techniques. To avoid metal scatter artefacts, we used moulded polymeric stem replicas provided by the manufacturer. These replicas had different surface and heat capacity characteristics than metal implants and could have presented small size and shape mismatches. We only investigated the Lubinus SP II stem with Palamed cement in a standardized setting. As such the conclusions drawn cannot be extrapolated to other stem types, other cement brands or other implantation modalities. Finally, only nine pairs of femora were analyzed. As such, and despite the large number of CT images, the study lacks power when the effect size is smaller than one and only “major” differences were statistically significant. On the other hand, some differences were small in absolute terms (< 0.5 mm) even if they were statistically significant and had a large effect size.

The exact clinical, mechanical and biological consequences of the stem implantation technique remain unclear. FEA models (7,12) suggest that the medullary canal-filling capacity of the stem and direct cortical bone support to the cement, improve mechanical implant stability despite larger areas of thin cement. On the other hand, larger line-to-line implants, result in more cement defects and could favour particle-induced osteolysis (1,8). For the Lubinus stem, this could be particularly detrimental because the highest incidence of such defects was found distally. Yet, it is unknown if in clinical practice, improved mechanical stem stability compensates for that potential “biological” drawback. Nevertheless, it is clear that excellent long-term results have been reported using both implantation philosophies (9,17,20). Further clinical and mechanical studies are needed to investigate the exact impact of stem-broach sizing on the long-term implant survival.

#### *Acknowledgments*

The authors wish to thank the department of Orthopaedic Surgery of the UZ Brussel for funding this study, Waldemar Link GmbH for providing polymeric Lubinus SP II replicas, Biomet for providing cement and vacuum mixing/pressurizing

systems, the department of Experimental and Human Anatomy of the VUB for providing proximal femurs, N. Buls, Medical Physicist at the UZ Brussel, for assessing the CT image quality, W. Duquet, Professor of Human Biometry at the VUB for his help with statistics and C. Van Paemel as well as P. Vandebussche for their technical support.

## REFERENCES

1. **Anthony PP, Gie GA, Howie CR.** Localised endosteal bone lysis in relation to femoral components of cemented total hip arthroplasty. *J Bone Joint Surg* 1990 ; 72-B : 971-979.
2. **Ayers D, Mann K.** The importance of proximal cement filling of the calcar region : A biomechanical justification. *J Arthroplasty* 2003 ; 18 : 103-109.
3. **Breusch SJ, Lukoschek M, Kreuzer J, Brocai D, Gruen TA.** Dependency of cement mantle thickness on femoral stem design and centralizer. *J Arthroplasty* 2001 ; 16 : 648-657.
4. **Crowninshield RD, Jennings JD, Laurent ML, Maloney WJ.** Cemented femoral component surface finish mechanics. *Clin Orthop* 1998 ; 355 : 90-102.
5. **Howell JR Jr., Blunt LA, Doyle C et al.** In vivo surface wear mechanisms of femoral components of cemented total hip arthroplasties : the influence of wear mechanism on clinical outcome. *J Arthroplasty* 2004 ; 19 : 88-101.
6. **Jacobsson SA, Ivarsson I, Djerf K, Wahlstrom O.** Stem loosening more common with ITH than Lubinus prosthesis. A 5-year clinical and radiographic follow-up of 142 patients. *Acta Orthop Scand* 1995 ; 66 : 425-431.
7. **Janssen D, van Aken J, Scheerlinck T, Verdonshot N.** Numerical analysis of the effect of cement philosophies on implant stability and cement fatigue failure. *Acta Orthop* (accepted November 2008).
8. **Jasty MJ, Floyd WE, Schiller AL, Goldring SR, Harris WH.** Localised osteolysis in stable, non-septic total hip arthroplasty. *J Bone Joint Surg* 1986 ; 68-A : 912-919.
9. **Langlais F, Kerboull M, Sedel L, Ling RSM.** The 'French Paradox'. *J Bone Joint Surg* 2003 ; 85-B : 17-20.
10. **Maher SA, Prendergast PJ.** Discriminating the loosening behaviour of cemented hip prostheses using measurements of migration and inducible displacement. *J Biomech* 2003 ; 35 : 257-265.
11. **Malchau H, Herberts P, Garrellick G, Söderman P, Eisler T.** Prognosis of total hip replacement. Update of results and risk-ratio. Analysis for revision and re-revision from the Swedish national hip arthroplasty register 1979-2000, 2002.
12. **Massin P, Astoin E, Lavaste F.** [Influence of proximal stem geometry and stem-cement characteristics on bone and cement stresses in femoral hip arthroplasty : finite element analysis] (in French). *Rev Chir Orthop* 2003 ; 89 : 134-143.
13. **Nivbrant B, Karrholm J, Soderlund P.** Increased migration of the SHP prosthesis : radiostereometric comparison with the Lubinus SP2 design in 40 cases. *Acta Orthop Scand* 1999 ; 70 : 569-577.
14. **O'Connor DO, Burke DW, Jasty M, Sedlacek RC, Harris WH.** In vitro measurement of strain in the bone cement surrounding the femoral component of total hip replacements during simulated gait and stair-climbing. *J Orthop Res* 1996 ; 14 : 769-777.
15. **Puolakka TJ, Pajamaki KJ, Halonen PJ et al.** The Finnish arthroplasty register : report of the hip register. *Acta Orthop Scand* 2001 ; 72 : 433-441.
16. **Scheerlinck T, Casteleyn P-P.** The use of primary total hip arthroplasties in university hospitals of the European Union. *Acta Orthop Belg* 2004 ; 70 : 231-239.
17. **Scheerlinck T, Casteleyn P-P.** Review article. The design features of cemented femoral hip implants. *J Bone Joint Surg* 2006 ; 88-B : 1409-1418.
18. **Scheerlinck T, de Mey J, Deklerck R.** In vitro analysis of the cement mantle of femoral hip implants : development and validation of a CT-scan based measurement tool. *J Orthop Res* 2005 ; 23 : 698-704.
19. **Scheerlinck T, de Mey J, Deklerck R, Noble PhC.** CT analysis of defects of the cement mantle and alignment of the stem. In vitro comparison of Charnley-Kerboul femoral hip implants inserted line-to-line and undersized in paired femora. *J Bone Joint Surg* 2006 ; 88-B : 19-25.
20. **Skinner JA, Todo S, Taylor M et al.** Should the cement mantle around the femoral component be thick or thin ? *J Bone Joint Surg* 2003 ; 85 : 45-51.
21. **Stolk J, Verdonshot N, Cristofolini L, Toni A, Huiskes R.** Finite element and experimental models of cemented hip joint reconstructions can produce similar bone and cement strains in pre-clinical tests. *J Biomech* 2002 ; 35 : 499-510.
22. **Wroblewski BM, Siney PD, Fleming PA, Bobak P.** The calcar femorale in cemented stem fixation in total hip arthroplasty. *J Bone Joint Surg* 2000 ; 82-B : 842-845.
23. **Zar JH.** *Biostatistical Analysis*. 3rd ed. Prentice Hall, Upper Saddle River, New Jersey, 1996.